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# **MACH CUTOFF ANALYSIS AND RESULTS FROM NASA'S FARFIELD INVESTIGATION OF NO-BOOM THRESHOLDS**

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Presented by:

Larry J. Cliatt, II

Authors:

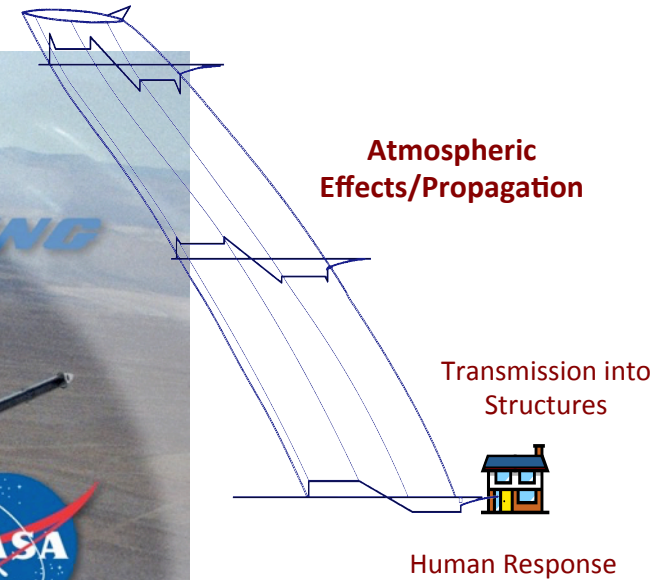
Larry J. Cliatt II, Michael A. Hill, Edward A. Haering, Jr.

*NASA Armstrong Flight Research Center*





# FARFIELD INVESTIGATION OF NO-BOOM THRESHOLDS (FAINT)







# NASA ARMSTRONG FLIGHT RESEARCH CENTER

*Armstrong Flight Research Center*

## Aeronautics Flight Research

- Over 60 years of flight research (NACA Muroc Flight Test Unit)
- Edwards Air Force Base (EAFB)
- Remote Location
- 350 Testable Days Per Year
- Extensive Range Airspace
- Supersonic Corridor





# TOPICS OF DISCUSSION

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- Motivation & Objectives
- Test Setup
- Flight Profile Planning
- Analysis
  - Mach cutoff calculations
  - Metrics for Mach cutoff acoustics
  - Noise levels due to Mach cutoff
  - Sensitivity Analysis
- Summary & Considerations





# MOTIVATION & BACKGROUND

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- **What is Mach Cutoff flight?**

- Supersonic flight when sonic boom rays do not reach the ground

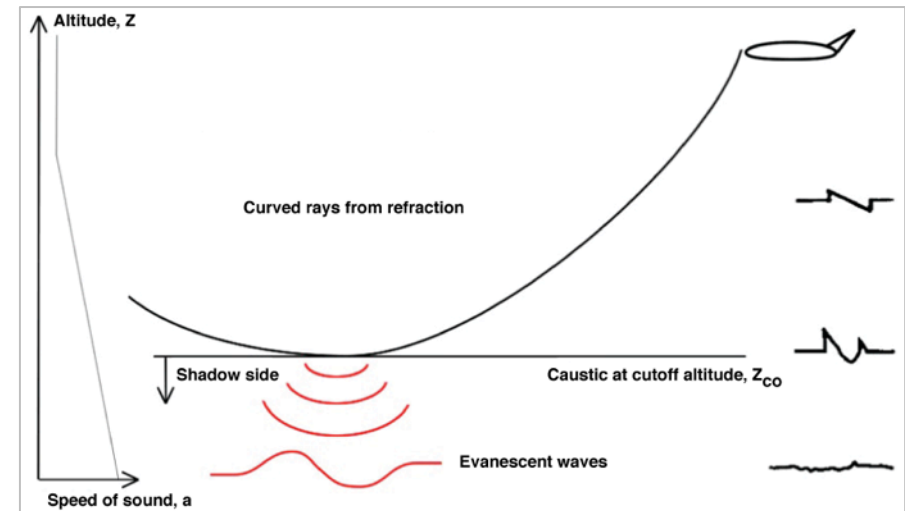
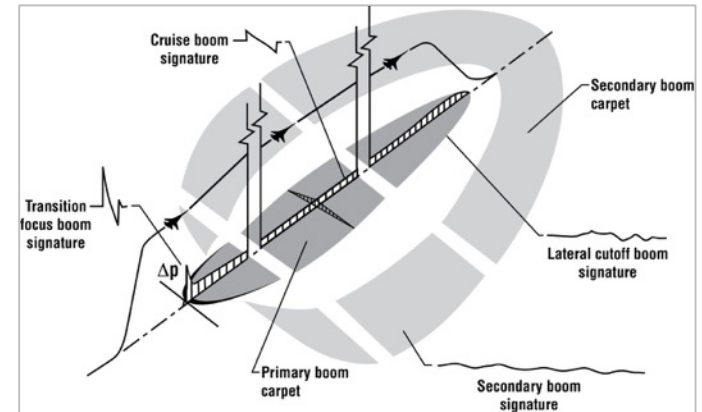
- Rays refract due mostly to temperature gradient

- **Commercial implications**

- “Boomless” flight

- Speeds up to Mach 1.3

- Increase in operations by over 30%

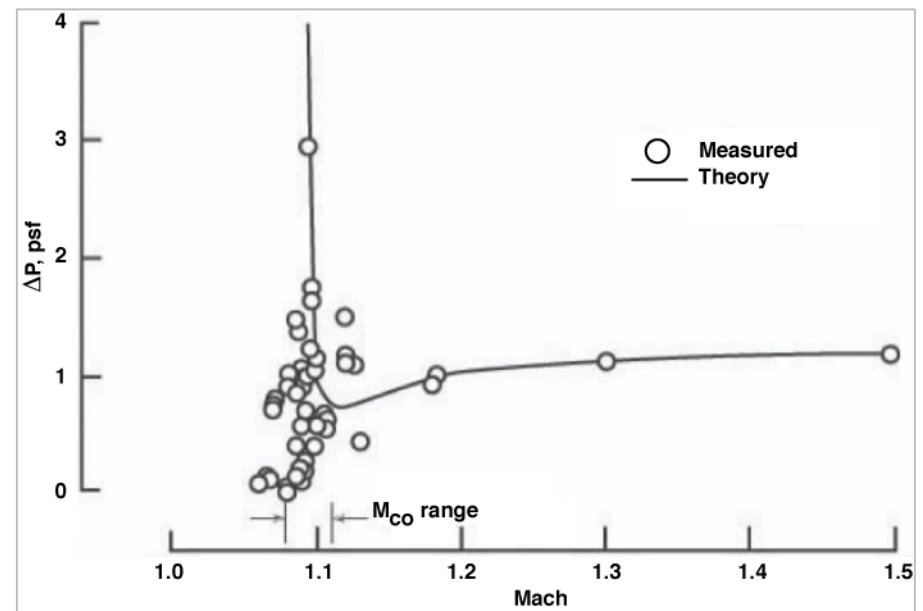




## MOTIVATION & BACKGROUND, *CONT.*

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- **Need:** Understanding of entire sonic boom envelope
- Change in ICAO/FAA regulations
- Notable noise due to Mach cutoff flight ( $M_{CO}$ )
- Inconclusive results from previous tests
- Limitations to common numerical predictions:
  - Based on geometrical acoustics
  - No solutions in shadow zones



Results from 1970 Bare Reactor Experiment, Nevada (BREN) study

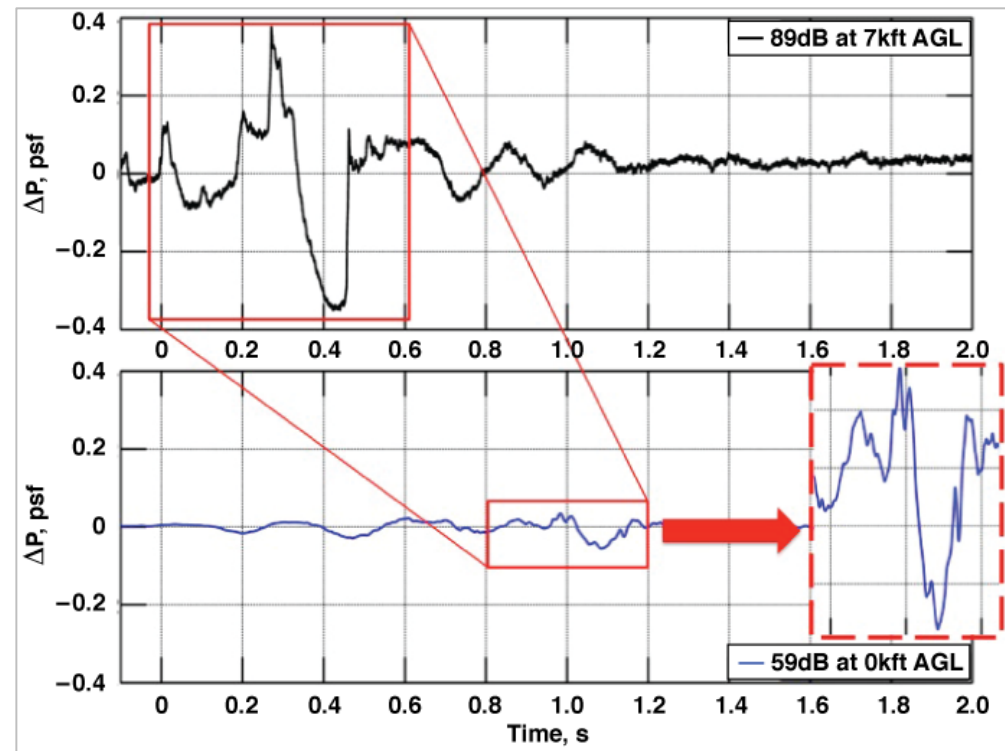




# PRIMARY OBJECTIVES

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- Study evanescent wave field
  - Finely spaced measurements
  - Attenuation and increase in signature length
  - Evanescent decay in shadow zone
- Design tools for flight planning and post-flight analysis
- Develop noise– $M_{CO}$  relationship
- Build database







# FLIGHT PROFILE PLANNING

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- Goal: Produce a range of cutoff altitudes ( $Z_{CO}$ ) between 2500 – 8000 ft (762.0 – 2438.4 m)
  - Assume initial flight altitude ( $Z$ ) and heading
  - Calculate required Mach ( $M$ )
- Rays refract above ground when their propagation speed ( $V_P$ ) exceeds the airplane ground speed ( $V_G$ ):

$$\frac{V_P}{V_G} \geq 1.0 \quad \text{where} \quad V_G = Ma_0 - u_{n_0} \quad (1)$$

$$V_P = \{a(Z) - u_n(Z)\} \quad (2)$$

$a$  : speed of sound  
 $u_n$  : wind speed direction of propagation  
 $0$  : subscript denotes at flight altitude

- Because  $V_P$  increases toward the ground:

$$Z_{CO} = Z @ \max \{V_P \geq V_G\} \quad (3)$$

- Use Eq. 1 to compute  $M$  that satisfies Eq. 3



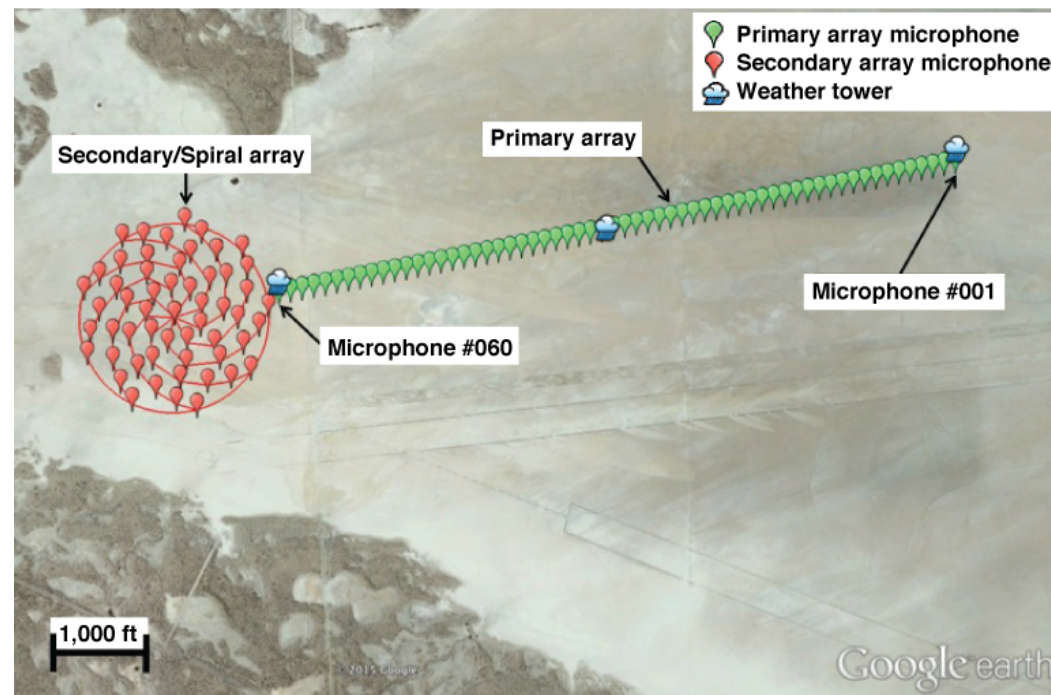




# TEST SETUP

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- Flight Conditions
  - F-18B airplane
  - Mach 1.128 – 1.174 and 34400 – 39300 ft (10.5 – 12.0 km) pressure altitude
- 7375 ft (2.2 km), 125 ft (38 m) spaced linear microphone array at 2300 ft (0.7 km) mean sea level
  - 60 microphones
- PCBoom<sup>1</sup> used for initial flight planning



<sup>1</sup> PCBoom was developed by Wyle (El Segundo, California)

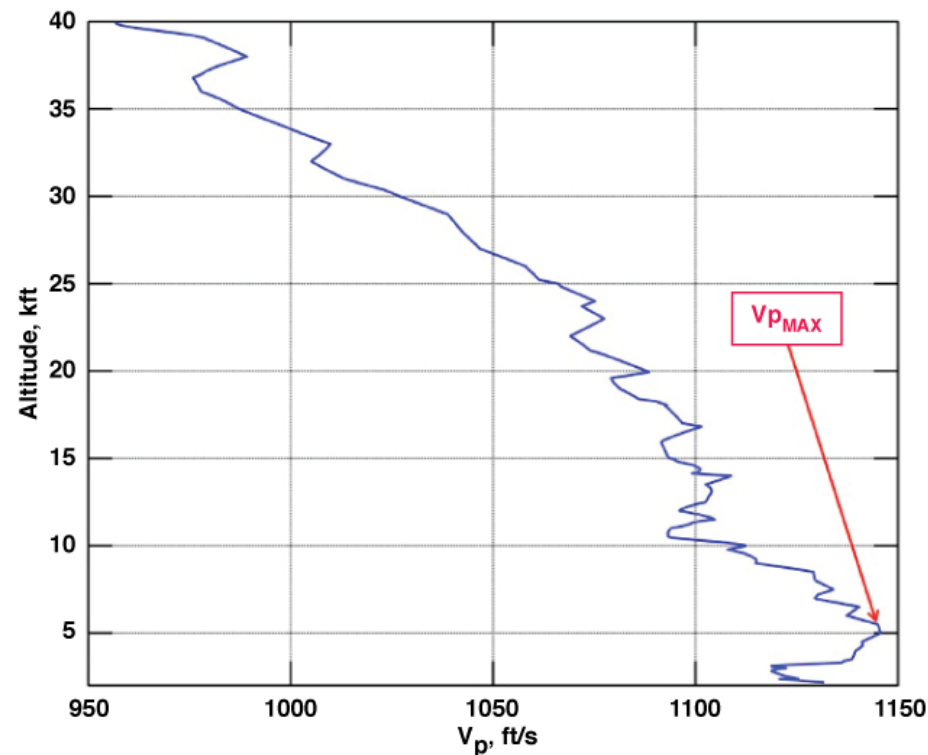


# MACH CUTOFF CALCULATIONS

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- Mach threshold ( $M_T$ ): Fastest Mach for  $M_{CO}$
- $M_T$  is independent of  $Z_{CO}$
- Dependent only on atmospheric conditions, mostly  $V_{P,max}$

$$M_T = \frac{1}{a_0} [V_{P_{MAX}} + u_{n_0}]$$

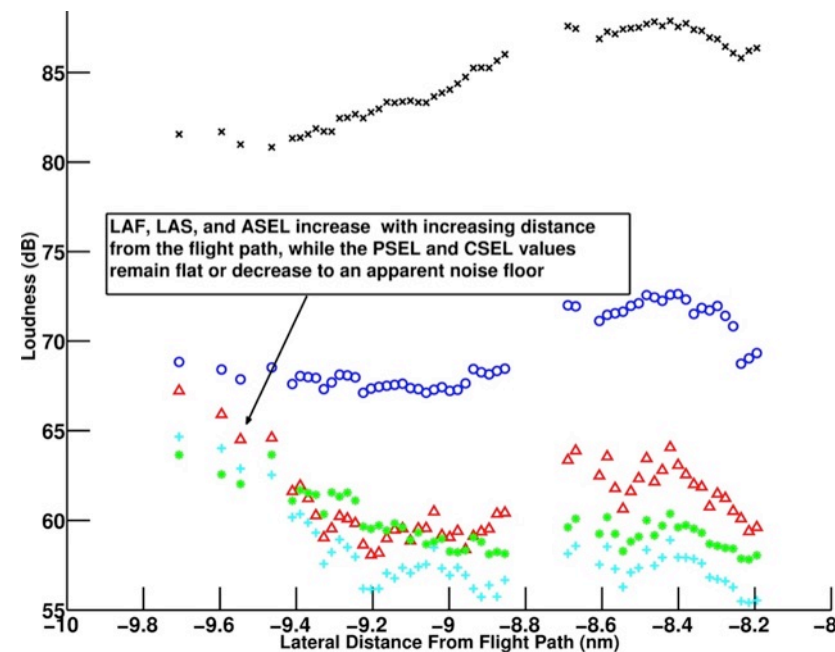
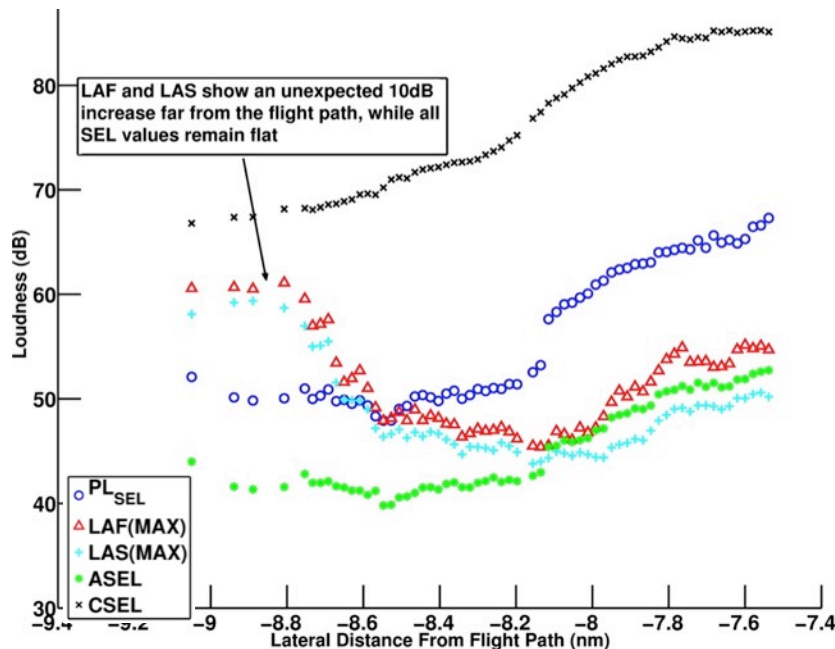
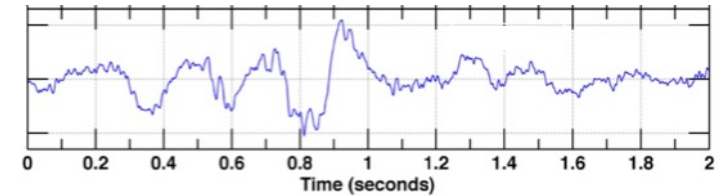




# METRICS FOR MACH CUTOFF ACOUSTICS

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- Overpressure alone not sufficient for sonic boom analysis
- Familiar metrics less applicable for waveforms near lateral cutoff and beneath Mach cutoff altitude due to variable duration and impulsiveness
- **Perceived Sound Exposure Level ( $PL_{SEL}$ )**
  - 99% energy windowing
  - Sound Exposure Level (SEL) 1-second normalized integration (ISO 1996)
  - Stevens' Mark VII Perceived Level weighting

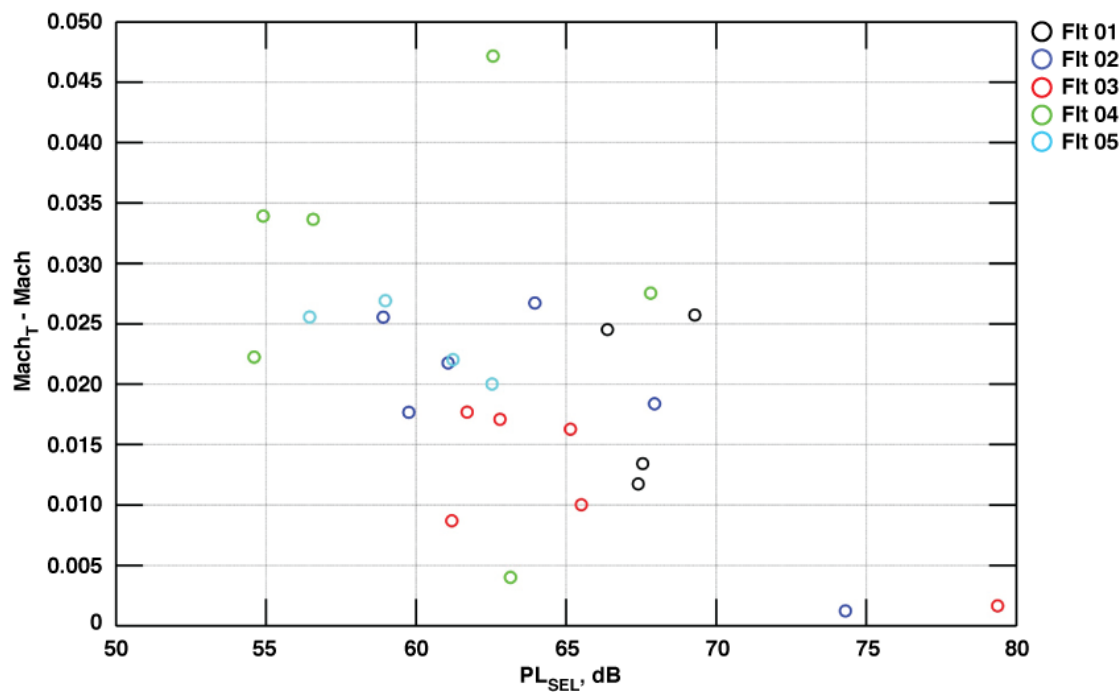




# NOISE LEVELS DUE TO MACH CUTOFF

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- New parameter:  $(M_T - M)$ 
  - Relates  $Z_{CO}$  to Mach number
  - More natural to commercial piloting operations
- However, correlation between  $(M_T - M)$  and noise on the ground ( $PL_{SEL}$ ) is indistinct due to varying  $Z_{CO}$



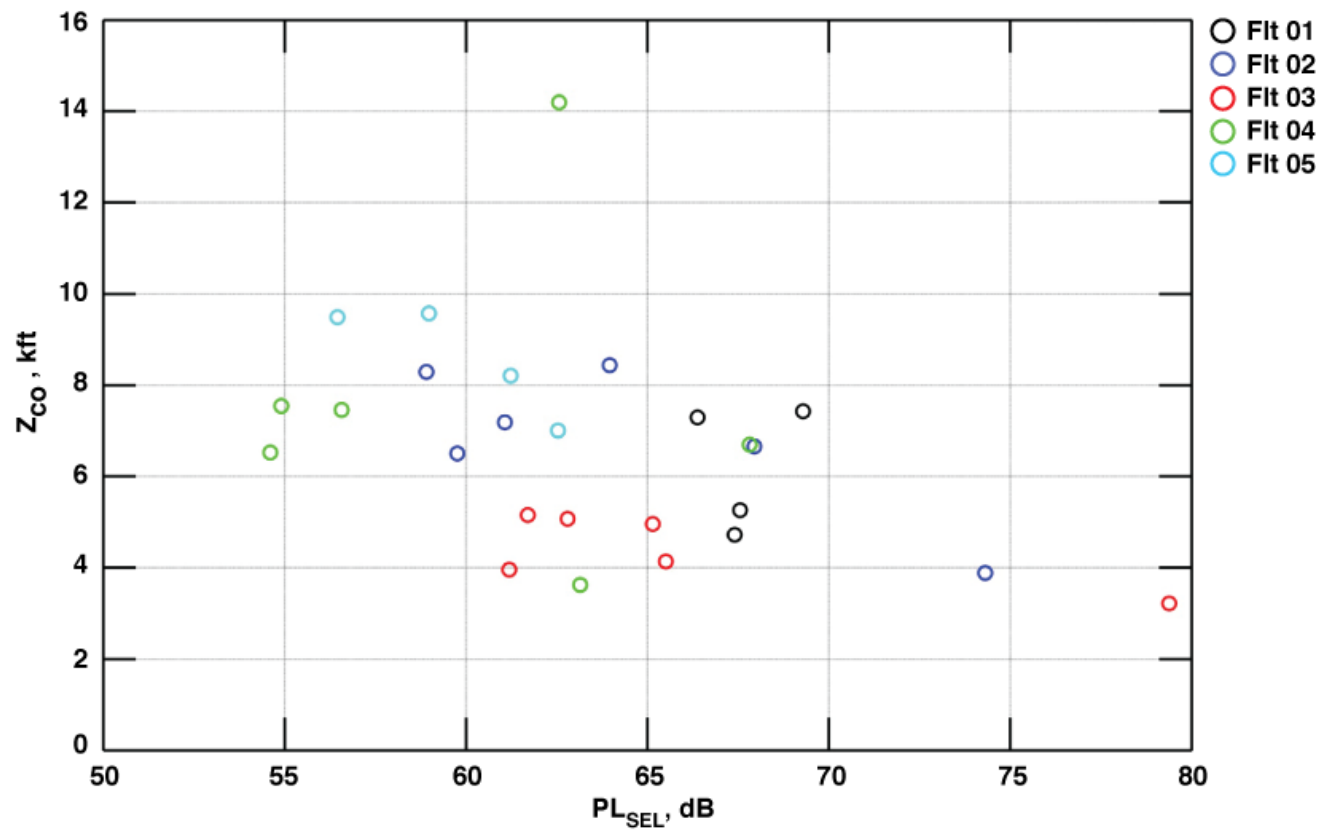




## NOISE LEVELS DUE TO MACH CUTOFF, *CONT.*

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- Correlation between  $Z_{CO}$  and  $PL_{SEL}$  is also indistinct
- Possibly due to sonic boom shock strength (Mach number)

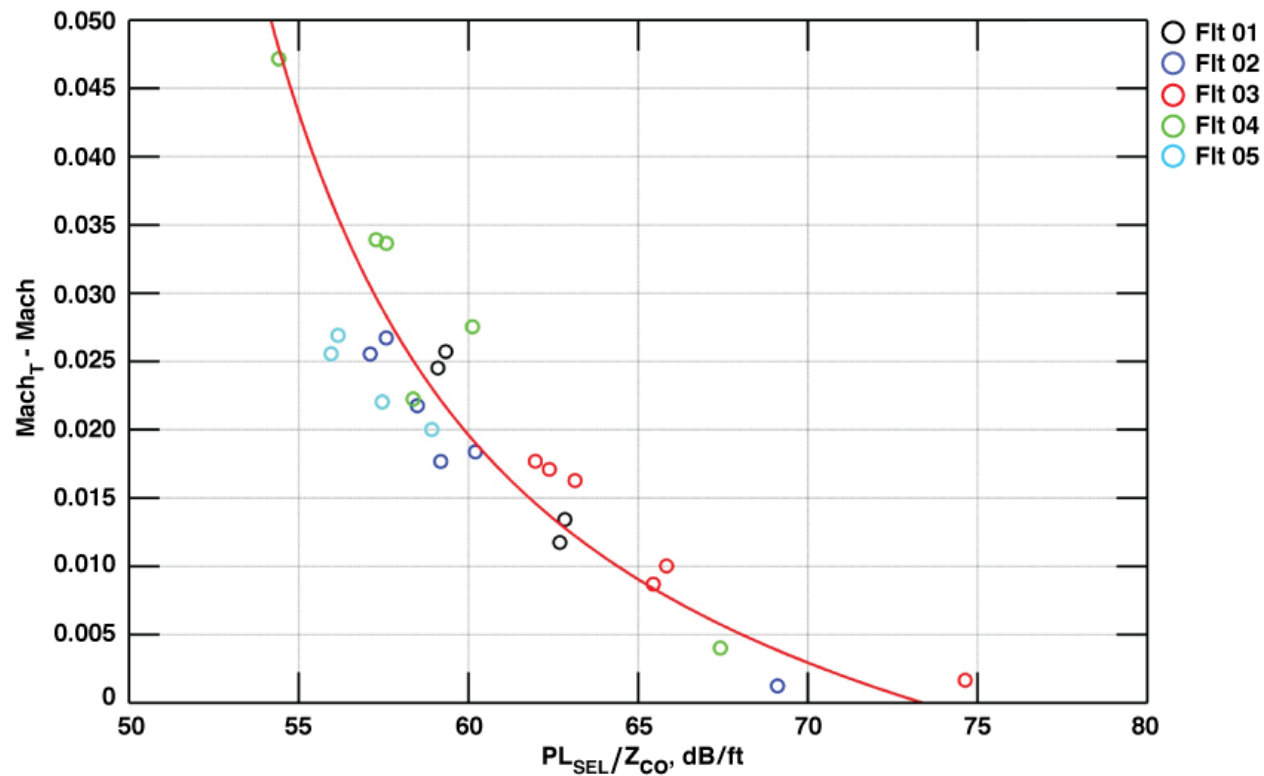




## NOISE LEVELS DUE TO MACH CUTOFF, *CONT.*

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- “Normalize” by  $Z_{CO}$
- **First known empirical model for shadow zone acoustics:**  $PL_{SEL} = f(M_T - M, Z_{CO})$
- Exponential decay fit → evanescent wave field

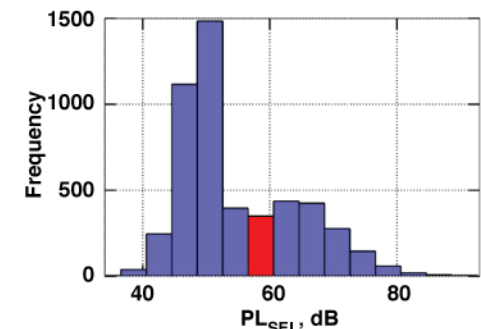
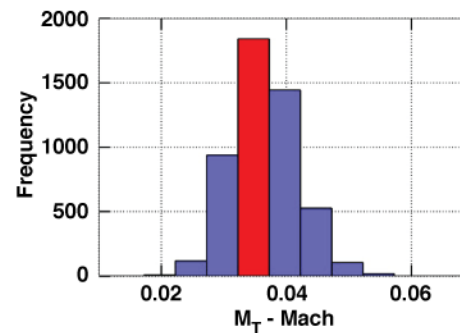
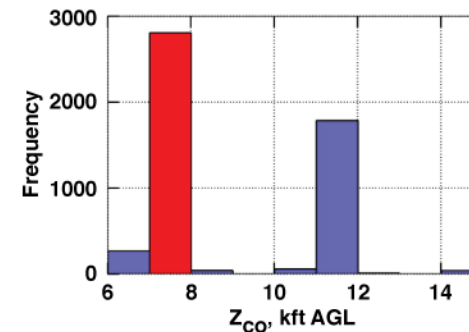
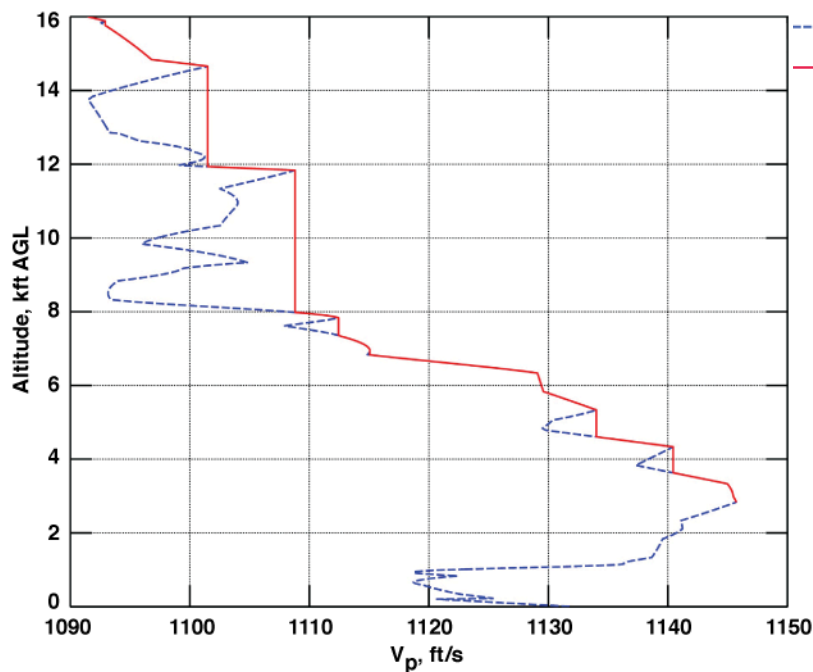




# SENSITIVITY ANALYSIS

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- Monte Carlo simulation of 5000  $M_{CO}$  cases
  - Constant Mach (1.135) and altitude 37000 ft (11277.6 m)
  - Random normal distribution of: wind speed ( $\sigma = 3$  knots), wind direction ( $\sigma = 10$  deg), and temperature ( $\sigma = 3$  °C)
- “Banding” of  $Z_{CO}$  due to “effective  $V_p$ ”



Red bars are as-flown values



## SUMMARY & CONSIDERATIONS

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- $PL_{SEL}$  shown to be a more consistent and applicable metric Mach cutoff sonic boom acoustics
- First known empirical model of Mach cutoff shadow zone acoustics allows:
  - The ability to predict sonic boom noise levels in real-time
  - Capability to design supersonic commercial airplane mission profiles for entire flight regime
  - Fast analysis. Computational models require significant computer core hours
- $M_{CO}$  is extremely sensitive to atmospheric changes
  - Commercial applications will require sophisticated flight planning tools







# FUTURE & ADDITIONAL WORK

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- Larger database to refine empirical model
- Verification of empirical model during flight
- Use model to validate computational codes, such as Gulfstream's Lossy Nonlinear Tricomi Equation (LNTE)
- Beamforming analysis (Boeing)



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**THANK YOU.**

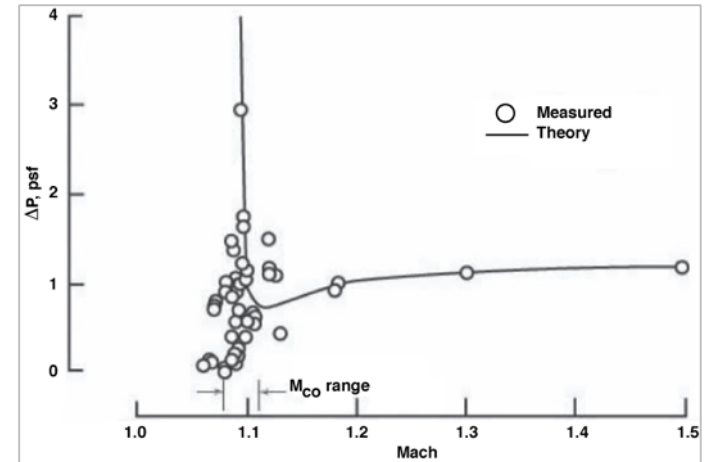
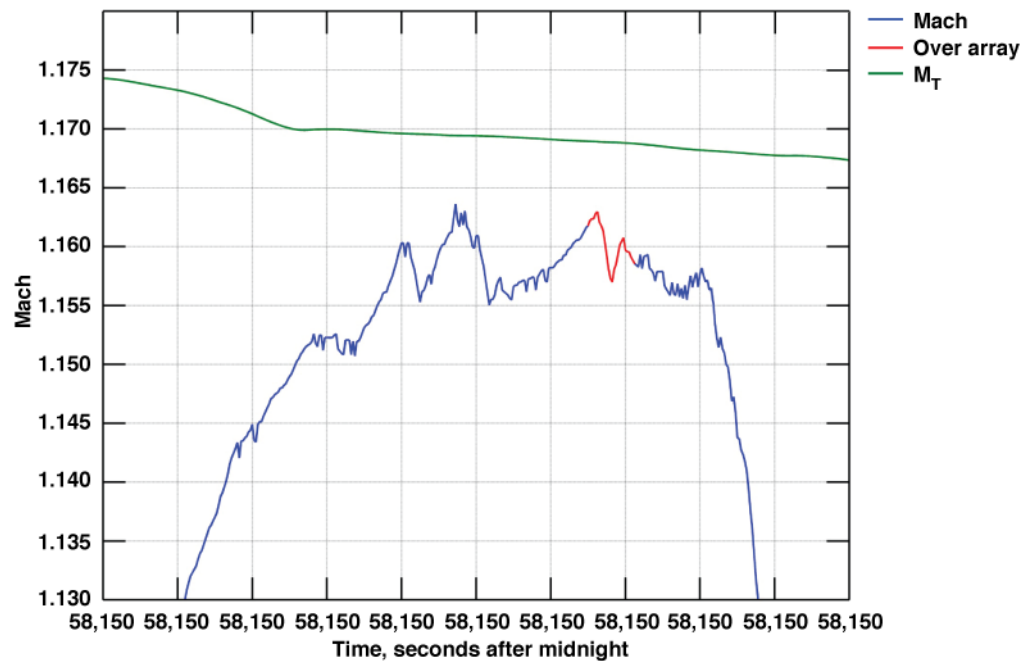




# MACH CUTOFF CALCULATIONS, *CONT.*

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- Importance of accurate windowing





## SENSITIVITY ANALYSIS, *CONT.*

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- Changes in both atmosphere and flight parameters

